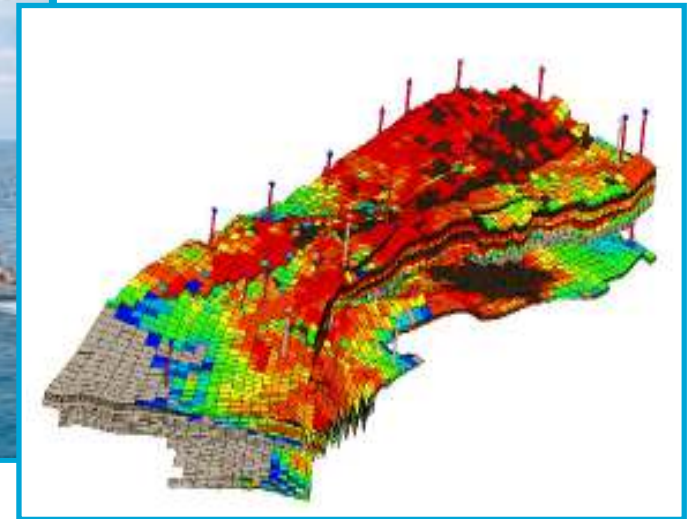


# Model-Reduced Variational Data Assimilation For Reservoir Model Updating



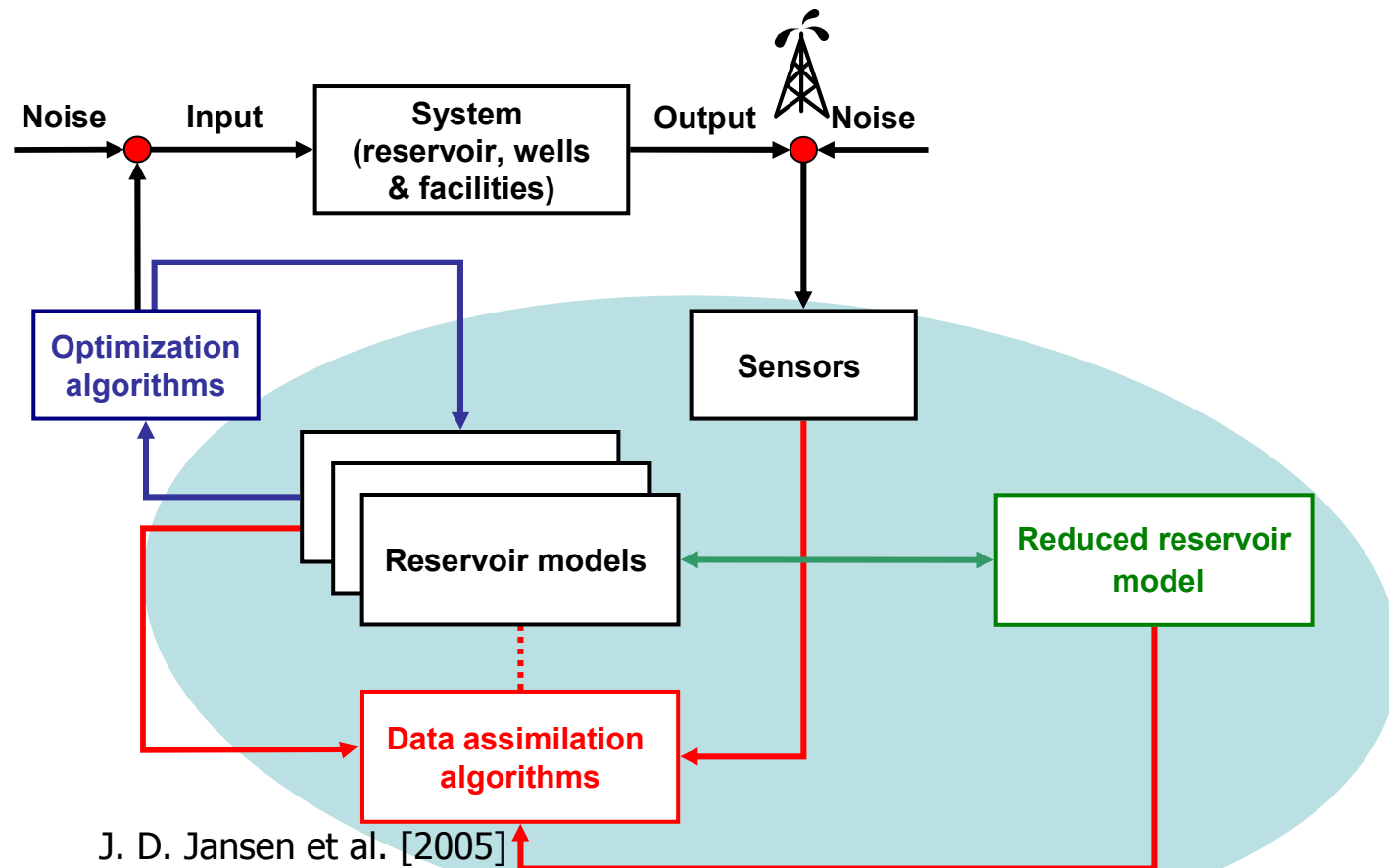
*M.P. Kaleta (TUD), A.W. Heemink (TUD), J.D. Jansen (TUD/Shell), R.G. Hanea (TUD/TNO)*

# Outline

- Background
- Model-reduced variational data assimilation (MRVDA)
- Study case
- Results
- Conclusions

# Background

Reservoir management represented as a model-based closed-loop controlled process



# Background

## Goal

To find the **maximum a posteriori estimate** of the log permeability field by solving the minimization problem:

$$\min_{\boldsymbol{\theta}} J(\boldsymbol{\theta}) = \frac{1}{2} (\boldsymbol{\theta} - \boldsymbol{\theta}^{prior})^T \mathbf{P}_{\boldsymbol{\theta}}^{-1} (\boldsymbol{\theta} - \boldsymbol{\theta}^{prior}) + \frac{1}{2} \sum_{i=1}^{N_D} (\mathbf{y}_i^{obs} - \mathbf{y}_i(\boldsymbol{\theta}))^T \mathbf{P}_i^{-1} (\mathbf{y}_i^{obs} - \mathbf{y}_i(\boldsymbol{\theta}))$$

- $\mathbf{y}_i^{obs}$ ,  $\mathbf{y}_i$  represent the vectors of observed and predicted production data at time  $t_i$ ,
- $\boldsymbol{\theta}$  the uncertain log permeability vector,
- $\boldsymbol{\theta}^{prior}$  the prior knowledge about log permeability,
- $\mathbf{P}_{\boldsymbol{\theta}}$  covariance matrix for the log permeability vector,
- $\mathbf{P}_i$  the covariance matrix for data measurements errors

# MRVDA

## Advantage of adjoint method

- A gradient based algorithm with gradient calculated by **adjoint method** which requires one adjoint solution regardless of the number of model parameters

## Disadvantage of adjoint method

- **Implementation of the adjoint model**

## Solutions

If we **re-parameterize the permeability field** then:

- we can calculate the gradient by perturbations: computationally expensive for large number of uncertain parameters
- we can construct the low-order approximation of the tangent linear reservoir model for which the low-order adjoint model is derived

# MRVDA

**Proper Orthogonal Decomposition** (Lumley 1967) also known as

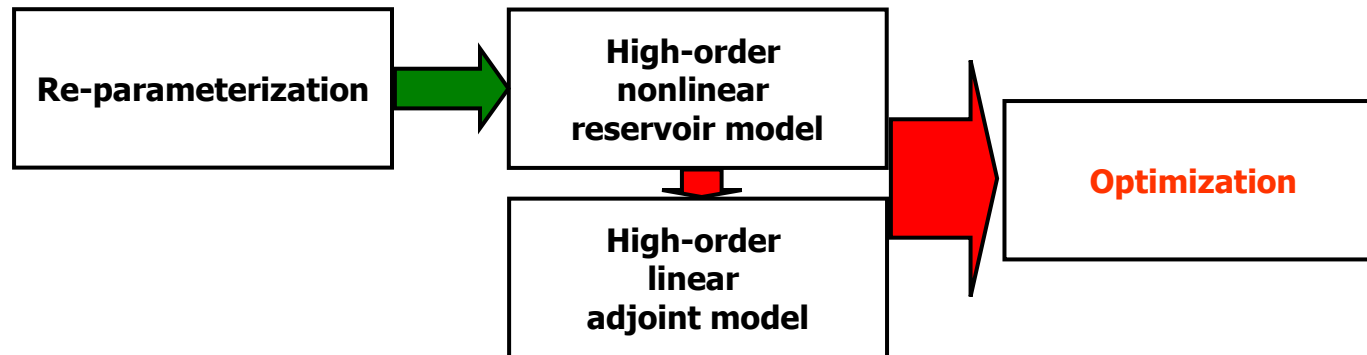
- Karhunen-Loève (K-L) Transform
  - Loève (1946)
  - Karhunen (1946)
- Empirical Orthogonal Function
- Principal Component Analysis (1986)

## Application

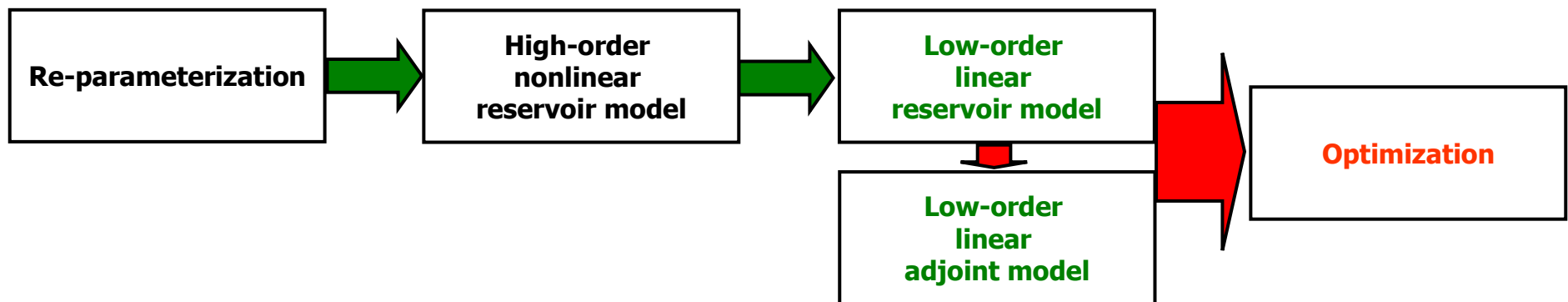
- Statistical tool to analyze experimental data
  - The POD is used to analyze the set of realizations with an aim to extract dominant features and trends (coherent structures called *patterns* in space)
- Reduced Order Modeling (ROM)
  - The POD is used to provide a relevant set of *basis functions* with which a low-dimensional subspace is identified, then the reduced model is constructed by projection of the governing equations on that subspace

# MRVDA

## Classical adjoint approach



## MRVDA



Vermeulen, P.T.M., Heemink, A.W. [2006]

Altaf, U.M., Inverse shallow water flow modeling

# MRVDA

High-order **nonlinear** model  high-order **linearized** model

Consider high-order **nonlinear** reservoir model

$$\mathbf{x}(t_i) = \mathbf{f}_i(\mathbf{x}(t_{i-1}), \boldsymbol{\theta}) \in \mathbf{R}^h, \quad h \ll O(10^6) \quad h_\theta = |\boldsymbol{\theta}| \ll O(10^6)$$

Tangent **linear** approximation of the high-order nonlinear reservoir model around  $(\mathbf{x}^b(t_i), \boldsymbol{\theta}^b)$  can be rewritten as

$$\Delta \mathbf{x}(t_i) = \frac{\partial \mathbf{f}_i(\mathbf{x}(t_{i-1}), \boldsymbol{\theta})}{\partial \mathbf{x}(t_{i-1})} \Delta \mathbf{x}(t_{i-1}) + \frac{\partial \mathbf{f}_i(\mathbf{x}(t_{i-1}), \boldsymbol{\theta})}{\partial \boldsymbol{\theta}} \Delta \boldsymbol{\theta}$$

where

$$\Delta \boldsymbol{\theta} = \boldsymbol{\theta} - \boldsymbol{\theta}^b \quad \text{and} \quad \Delta \mathbf{x}(t_i) = \mathbf{x}(t_i) - \mathbf{x}^b(t_i)$$

## Step 0

Re-parameterize permeability field using set of realizations  $\Theta = \{\boldsymbol{\theta}_1, \dots, \boldsymbol{\theta}_{K_\theta}\}$

$$\Delta \boldsymbol{\theta} = \mathbf{P}^\theta \mathbf{r}^\theta, \quad \mathbf{r}^\theta \in \mathbf{R}^{l_\theta}, \quad l_\theta \ll h_\theta$$



# MRVDA

High-order linearized model  low-order model

## Step 1

Generate number of system solutions and define *snapshots* as

$$\Delta \mathbf{x}(t_i) = \mathbf{f}_i(\mathbf{x}(t_{i-1}), \boldsymbol{\theta}^b + \mathbf{P}^\theta \mathbf{r}^\theta) - \mathbf{f}_i(\mathbf{x}^b(t_{i-1}), \boldsymbol{\theta}^b)$$

## Step 2

Apply POD on pressure and saturation snapshots separately and use it to derive projection subspace

$$\Delta \mathbf{x}(t_i) \approx \mathbf{P} \mathbf{r}(t_i) \quad \mathbf{r} \in \mathbf{R}^l, l \ll h$$

Project the **high-order** linearized model

$$\Delta \mathbf{x}(t_i) = \frac{\partial \mathbf{f}_i(\mathbf{x}(t_{i-1}), \boldsymbol{\theta})}{\partial \mathbf{x}(t_{i-1})} \Delta \mathbf{x}(t_{i-1}) + \frac{\partial \mathbf{f}_i(\mathbf{x}(t_{i-1}), \boldsymbol{\theta})}{\partial \boldsymbol{\theta}} \Delta \boldsymbol{\theta}$$

into **low-order** linear model

$$\mathbf{r}(t_i) = \mathbf{N}_i \mathbf{r}(t_{i-1}) + \mathbf{N}_i^\theta \mathbf{r}^\theta$$

# MRVDA

## Step 3

**Approximate** the matrices of the low-order model

$$\mathbf{N}_i = \mathbf{P}^T \frac{\partial \mathbf{f}_i(\mathbf{x}(t_{i-1}), \boldsymbol{\theta})}{\partial \mathbf{x}(t_{i-1})} \mathbf{P} \in \mathbf{R}^{l \times l} \quad \mathbf{N}_i^\theta = \mathbf{P}^T \frac{\partial \mathbf{f}_i(\mathbf{x}(t_{i-1}), \boldsymbol{\theta})}{\partial \boldsymbol{\theta}} \mathbf{P}^\theta \in \mathbf{R}^{l \times l_\theta}$$

Using the chain rule differentiation

$$\frac{\partial \mathbf{f}_i(\mathbf{x}^b(t_{i-1}) + \mathbf{P}\mathbf{r}_j(t_{i-1}), \boldsymbol{\theta}^b)}{\partial \mathbf{r}_j(t_{i-1})} = \frac{\partial \mathbf{f}_i(\mathbf{x}^b(t_{i-1}) + \mathbf{P}\mathbf{r}_j(t_{i-1}), \boldsymbol{\theta}^b)}{\partial \mathbf{x}(t_{i-1})} \frac{\partial \mathbf{x}(t_{i-1})}{\partial \mathbf{r}_j(t_{i-1})} = \frac{\partial \mathbf{f}_i(\mathbf{x}^b(t_{i-1}) + \mathbf{P}\mathbf{r}_j(t_{i-1}), \boldsymbol{\theta}^b)}{\partial \mathbf{x}(t_{i-1})} \mathbf{P}_j$$

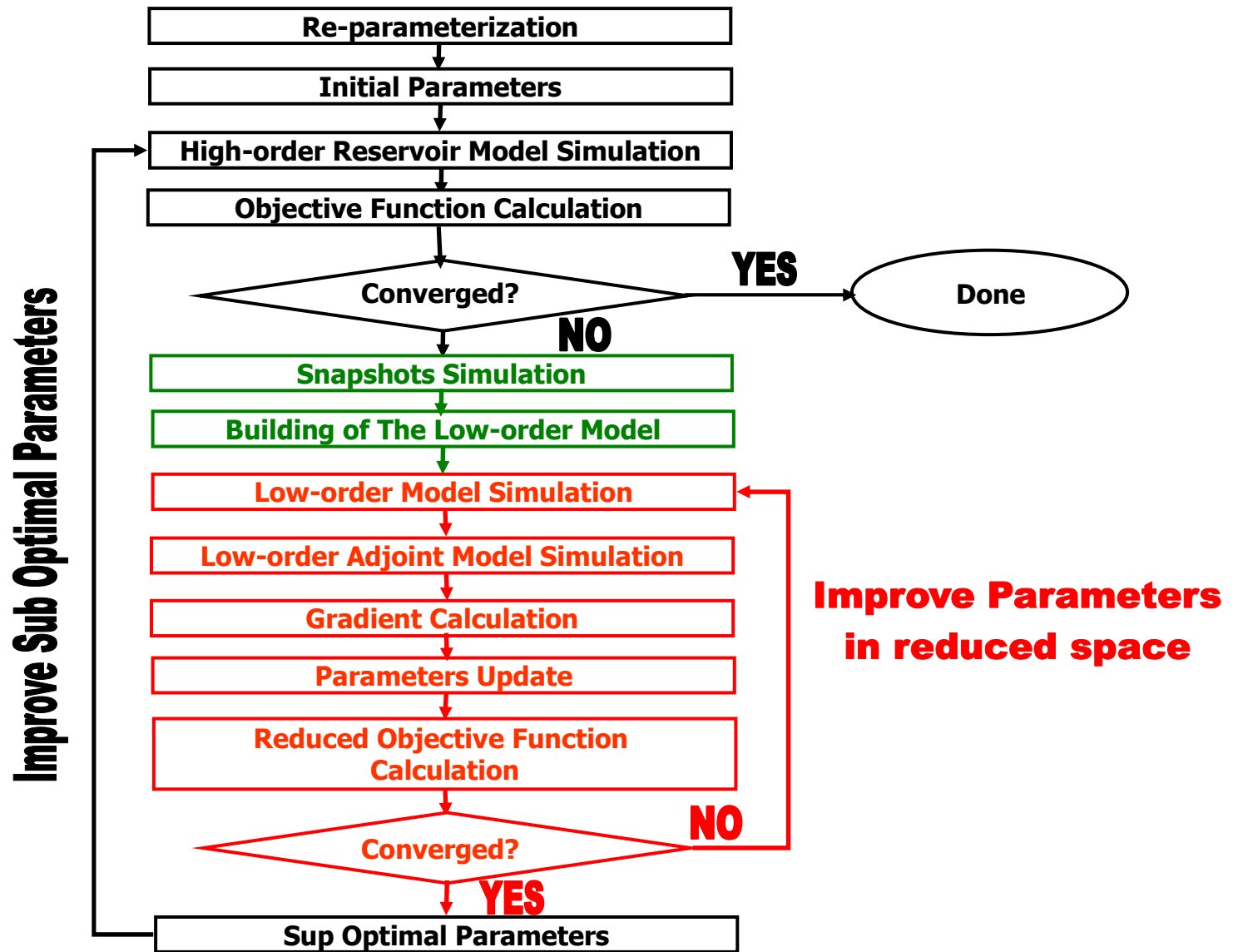
$$\frac{\partial \mathbf{f}_i(\mathbf{x}^b(t_{i-1}), \boldsymbol{\theta}^b + \mathbf{P}^\theta \mathbf{r}_j^\theta)}{\partial \mathbf{r}_j^\theta} = \frac{\partial \mathbf{f}_i(\mathbf{x}^b(t_{i-1}), \boldsymbol{\theta}^b + \mathbf{P}^\theta \mathbf{r}_j^\theta)}{\partial \boldsymbol{\theta}} \frac{\partial \boldsymbol{\theta}}{\partial \mathbf{r}_j^\theta} = \frac{\partial \mathbf{f}_i(\mathbf{x}^b(t_{i-1}), \boldsymbol{\theta}^b + \mathbf{P}^\theta \mathbf{r}_j^\theta)}{\partial \mathbf{r}_j^\theta} \mathbf{P}_j^\theta$$

Using **finite difference approximation** we get

$$\frac{\partial \mathbf{f}_i(\mathbf{x}^b(t_{i-1}), \boldsymbol{\theta}^b)}{\partial \mathbf{x}(t_{i-1})} \mathbf{P}_j \approx \frac{\mathbf{f}_i(\mathbf{x}^b(t_{i-1}) + \varepsilon \mathbf{P}_j, \boldsymbol{\theta}^b) - \mathbf{f}_i(\mathbf{x}^b(t_{i-1}), \boldsymbol{\theta}^b)}{\varepsilon}$$

$$\frac{\partial \mathbf{f}_i(\mathbf{x}^b(t_{i-1}), \boldsymbol{\theta}^b)}{\partial \boldsymbol{\theta}} \mathbf{P}_j^\theta \approx \frac{\mathbf{f}_i(\mathbf{x}^b(t_{i-1}), \boldsymbol{\theta}^b + \varepsilon^\theta \mathbf{P}_j^\theta) - \mathbf{f}_i(\mathbf{x}^b(t_{i-1}), \boldsymbol{\theta}^b)}{\varepsilon^\theta}$$

# MRVDA

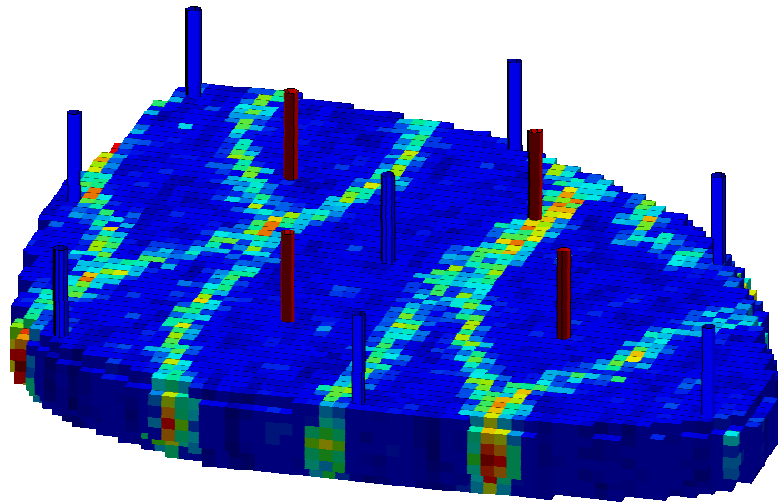


# MRVDA

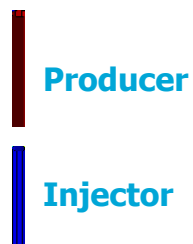
## Computational complexity

- Preprocessing cost of **generating representative snapshots** spanning a large portion of possible permeability field
  
- Preprocessing cost of **solving eigenvalue problems**
  
- Preprocessing cost of **building low-order system matrices**
  - As many model runs + multiplications of Jacobians with projection matrix as many state patterns
  - As many model runs + multiplications of Jacobians with projection matrix as many parameters
  
- The cost of **solving dense low-order linear model**

# Study case



Gijs van Essen [2006]



## Reservoir model assumption

- 3 dimensional (60x60x7 with 18553 active grid blocks)
- Two-phase (oil-water)
- No-flow boundaries at all sides

## Measurements

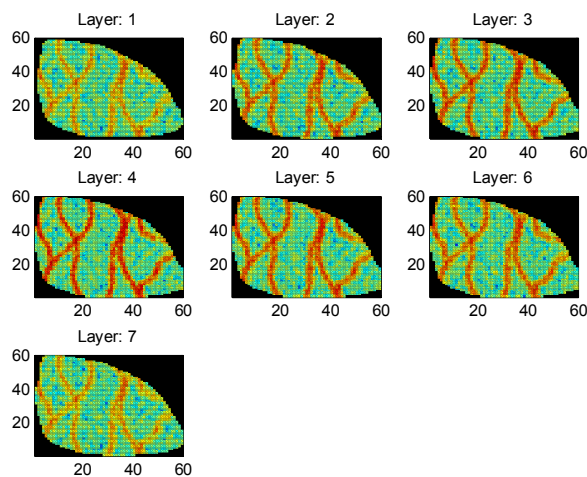
- Bottom hole pressures from injectors each 60 days during 3 years
- Flow rates from producers each 60 days during 3 years

# Results

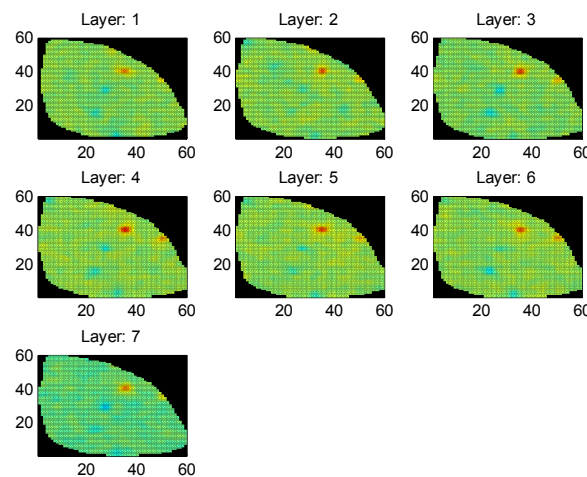
## Model-Reduced VDA

Outer loop	Nr of model simulations	Objective function	Permeability patterns	State patterns	Number of snapshots
0	-	270	22	-	-
1	~ 67	130	22	29+5	200

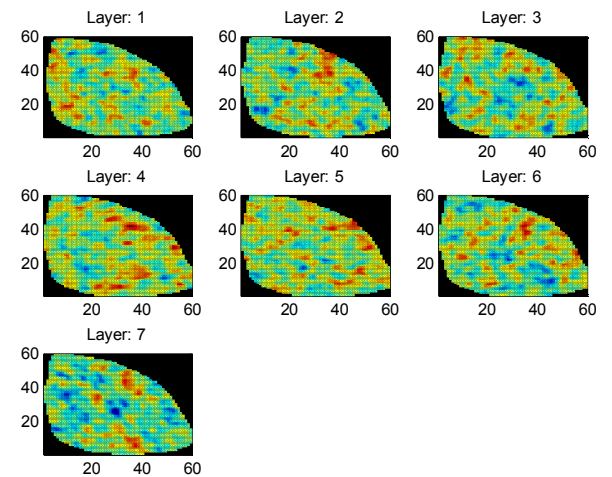
True log perm field



Prior log perm field

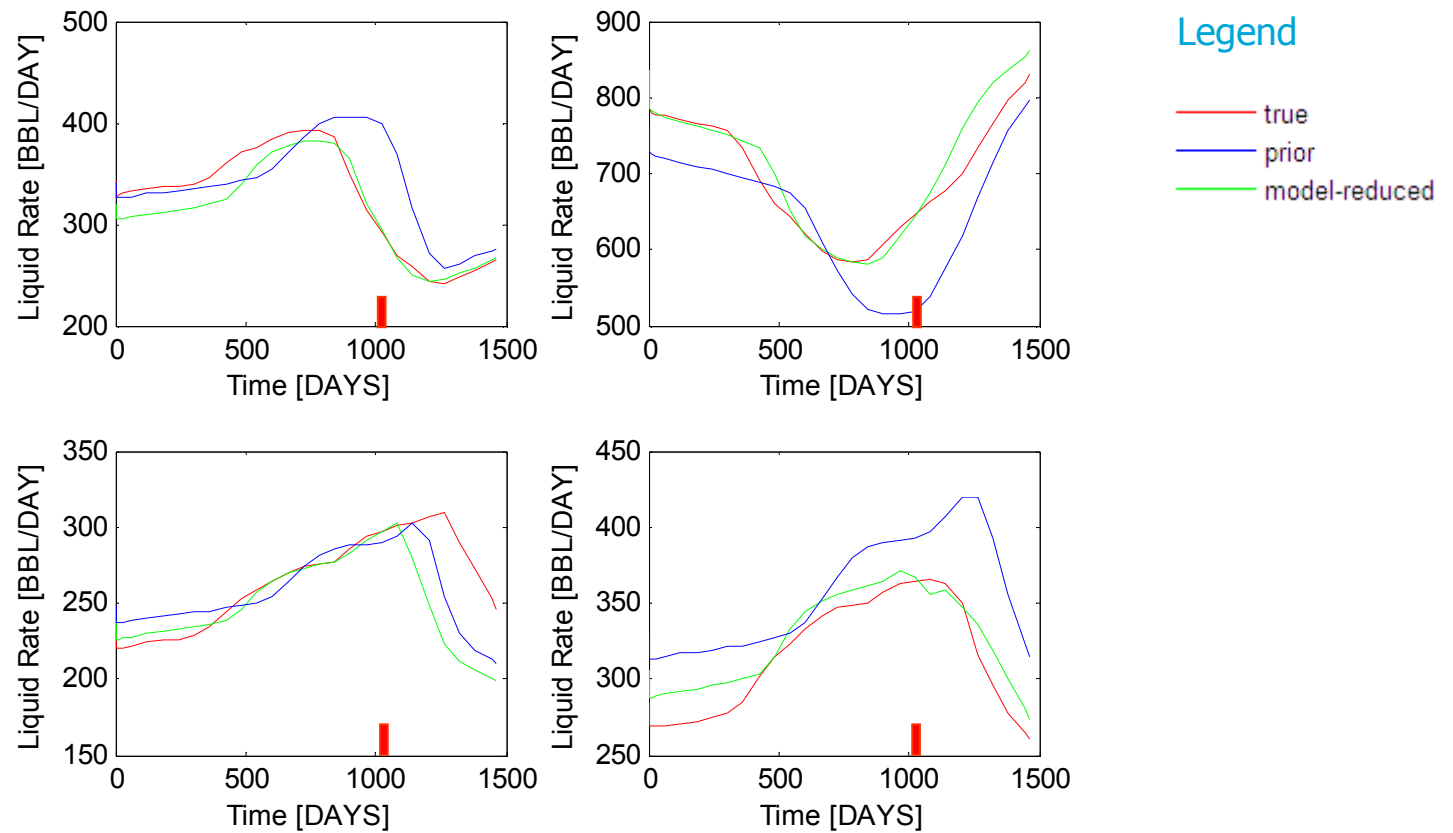


Estimated log perm field



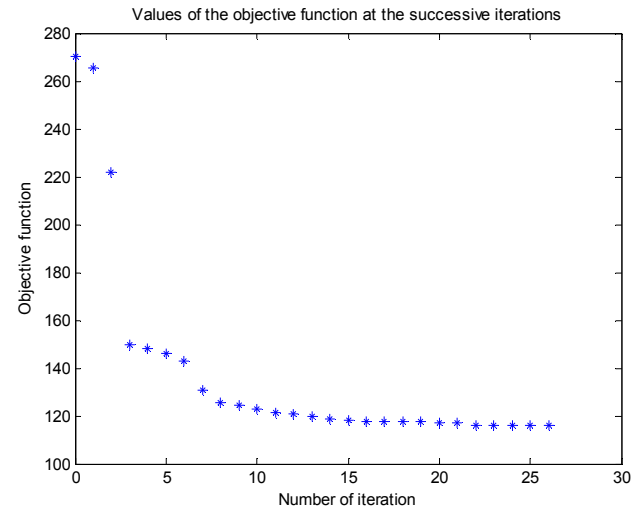
# Results

## Liquid rate in the production wells

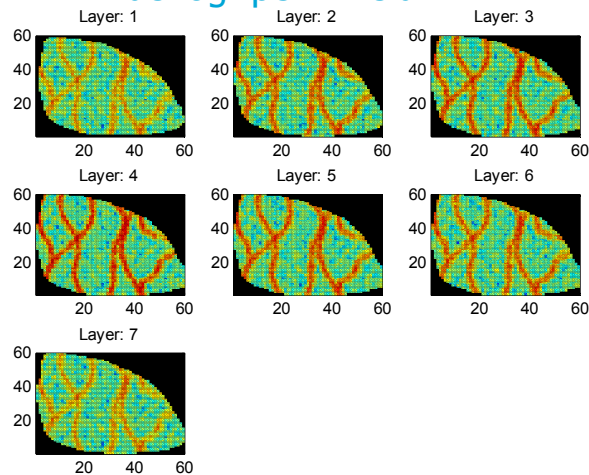


# Results

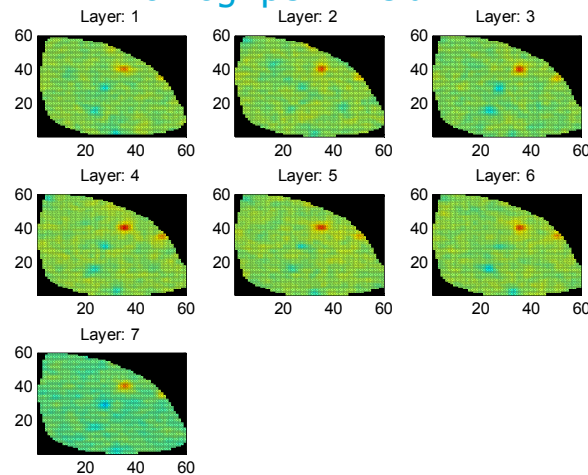
## Classical adjoint approach



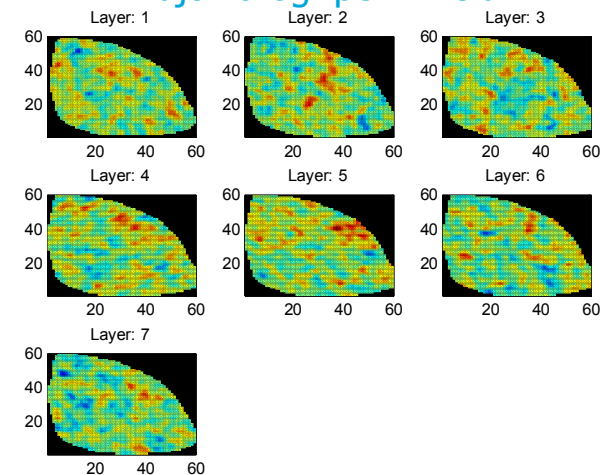
True log perm field



Prior log perm field



Adjoint log perm field



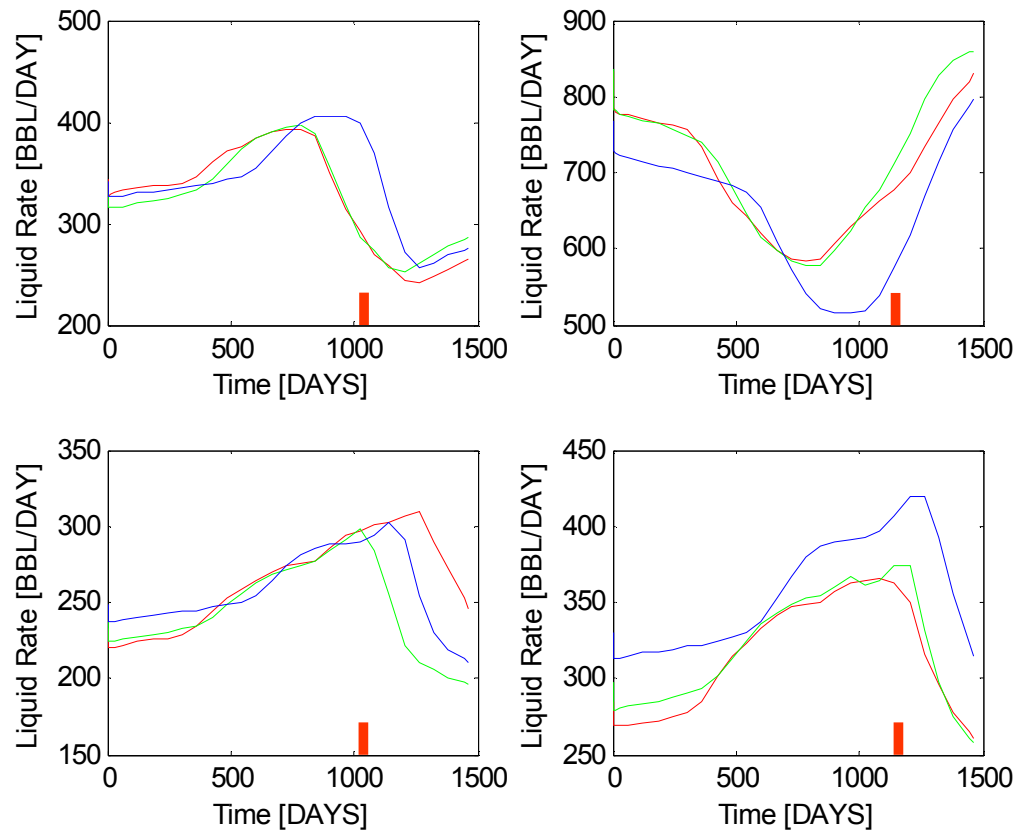


# Results

## Liquid rate in the production wells

### Legend

- true
- prior
- adjoint

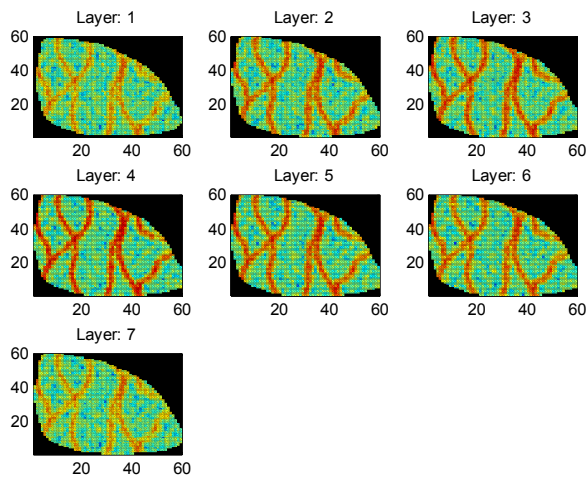


# Results

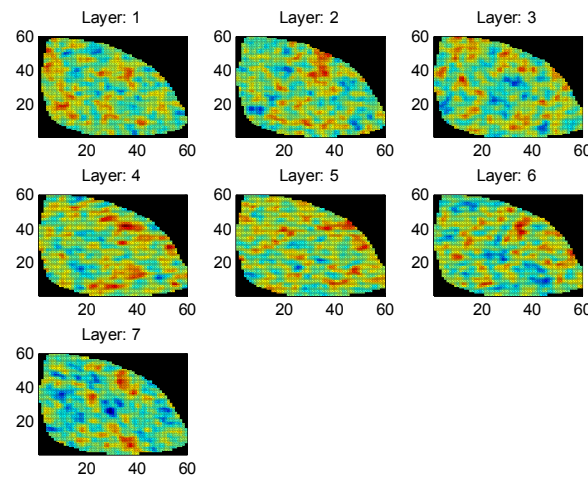
## Comparison of the methods

Method	Objective function	Time in simulations
Initial (Prior)	270	-
Model-reduced approach	130	~67
Adjoint approach	116	~26*2

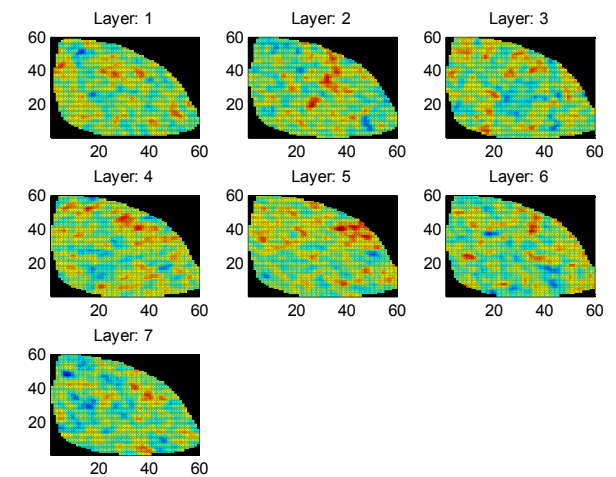
True log perm field



Model-reduced log perm field



Adjoint log perm field



# Conclusions

- Model-reduced variational data assimilation **does not require the implementation of the adjoint of the tangent linear model of the original reservoir model**
- Model-reduced variational data assimilation gives the estimates comparable to those from data assimilation using an adjoint method (comparable match and predictions)
- Model-reduced variational data assimilation is easy to implement and treats simulator as a black-box
- **If we have the adjoint code then we do go for the classical approach**

Questions?

# MRVDA: Proper Orthogonal Decomposition

Suppose we have an ensemble

$$\mathbf{X} = \{\mathbf{x}_1, \dots, \mathbf{x}_K\} \quad \mathbf{x}_i \in \mathbf{R}^h, \quad h \ll O(10^6)$$

POD seeks for *the best / optimal* linear representations of the members of the set  $\mathbf{X}$  :

$$\mathbf{X} \approx \hat{\mathbf{X}} = [\hat{\mathbf{x}}_1, \dots, \hat{\mathbf{x}}_K]_{h \times K} = [\mathbf{p}_1, \dots, \mathbf{p}_l]_{h \times l} \begin{bmatrix} r_1^1 & \dots & r_K^1 \\ \vdots & \ddots & \vdots \\ r_1^l & \dots & r_K^l \end{bmatrix}_{l \times K} \quad \mathbf{p}_i \in \mathbf{R}^h$$

## Optimality condition

$$\min_{\mathbf{P} \in \mathbf{R}^{h \times l}} \frac{1}{K} \sum_{i=1}^K \|\mathbf{x}_i - \mathbf{P}\mathbf{P}^T \mathbf{x}_i\|_2$$

## Solution

The above optimization problem is solved by **eigenvalue analysis** of the correlation matrix  $\mathbf{R} = \mathbf{X}\mathbf{X}^T$ , that is

$$\mathbf{X}\mathbf{X}^T \mathbf{p}_i = \lambda_i \mathbf{p}_i$$

# MRVDA: Proper Orthogonal Decomposition

*An optimal basis* is given by

$$\mathbf{P}^* = [\mathbf{p}_1, \mathbf{p}_2, \dots, \mathbf{p}_l]$$

where  $\mathbf{p}_i$  is the eigenvector corresponding to  $i$ -th largest eigenvalue  $\lambda_1 \geq \lambda_2 \geq \dots \geq \lambda_l \geq \dots \geq \lambda_K \geq 0$  of the matrix

The relative importance present in each basis vector

$$\varphi_j = \frac{\lambda_j}{\sum_{i=1}^K \lambda_i}$$

Choose  $l$  such that

$$\sum_{i=1}^l \varphi_i \leq \alpha$$

where  $\alpha$  denotes the fraction of the cumulative relative importance we want to capture

# MRVDA: Reduced Order Modeling

Consider a general **high-order** nonlinear discrete reservoir system

$$\mathbf{x}(t_i) = \mathbf{f}_i(\mathbf{x}(t_{i-1}), \boldsymbol{\theta}) \in \mathbf{R}^h,$$

$$\mathbf{y}(t_i) = \mathbf{h}_i(\mathbf{x}(t_i), \boldsymbol{\theta})$$

The aim of the **reduced order modeling** is to find the projection  $\mathbf{P} \in \mathbf{R}^{h \times l}$  with  $\mathbf{P}^T \mathbf{P} = \mathbf{I}_l$  and  $h \ll O(10^6)$  where  $l \ll h$  to obtain the **low-order** system

$$\mathbf{r}(t_i) = \mathbf{P}^T \mathbf{f}_i(\mathbf{P} \mathbf{r}(t_{i-1}), \boldsymbol{\theta})$$

$$\mathbf{y}(t_i) = \mathbf{h}_i(\mathbf{P} \mathbf{r}(t_i), \boldsymbol{\theta})$$

whose trajectories  $\mathbf{r}(t_i) = \mathbf{P}^T \mathbf{x}(t_i)$  evolve in  $l$ -dimensional space

